

UNIVERSITY OF EAST SARAJEVO FACULTY OF MECHANICAL ENGINEERING



6th INTERNATIONAL SCIENTIFIC CONFERENCE



COMETa 2022

"Conference on Mechanical Engineering Technologies and Applications"

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17th-19th November East Sarajevo, RS, B&H

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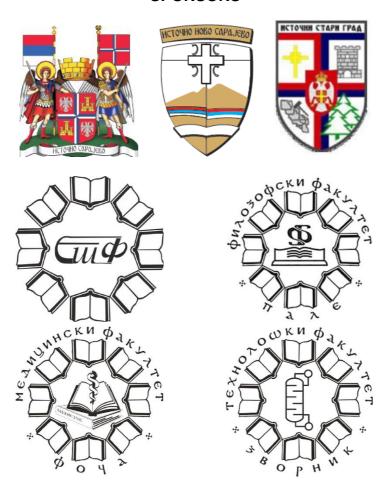
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PREFACE

The economic power of a society can be expressed by different indicators. However, it is certain that the competitiveness of the economy is one of the most important. In this sense, it is necessary for industrial production to follow modern development trends, which are based on current scientific achievements. Only a holistic approach in the application of knowledge in various engineering fields, and especially in the field of mechanical engineering, is a guarantee of economic progress, which enables long-term stability and prosperity of each country. Precisely for these reasons, the Faculty of Mechanical Engineering of the University of East Sarajevo organized the 1st International Scientific Conference COMETa in 2012, and this year is its 6th edition.

The main goal of the conference is to strengthen cooperation with the academic community, scientific-research institutions and, above all, with business entities. Conference COMETa 2022 is an opportunity for all participants to offer guidelines and create a better environment for more intensive industrial development through the exchange of knowledge and experience. That is going to have impact to increasing the competitiveness of national economic entities on the foreign market. The participation of a significant number of domestic and foreign scientists and researchers strengthens our conviction that in the near future we will be able to overcome challenges that are present in the technical-technological development of an advanced society in the 21st century, mainly through the generation of new ideas and the introducing of modern approaches to solving complex tasks in the field of mechanical engineering. In this sense, all your proposals and suggestions are more than welcome and will be carefully considered by the Scientific and Organizing Committee in order to improve the organization of the next conferences. Acknowledging the importance of the wide field of mechanical engineering for the overall industrial development of society, the work of the conference will take place through 7 sections, including the Student section. The program is focused on the following thematic areas:

- Manufacturing technologies and advanced materials,
- Applied mechanics and mechatronics,
- Machine design, simulation and modeling,
- Product development and mechanical systems,
- Energy and thermotechnic,
- Renewable energy and environmental protection,
- Maintenance and technical diagnostics,
- Quality, management and organization.

At this year's conference COMETa 2022, 105 papers including 4 plenary lectures will be published in the Proceedings.

We are specially looking forward that conference registered a record number of participants from abroad. Namely, 300 authors come from 25 countries. This is certainly the result of strenuous activities that were aimed at raising the international reputation and visibility of the conference in the regional, but also in the wider academic and scientific research space, which will be one of the primary goals in the future.

On behalf of the Organizing Committee of the conference COMETa 2022, we express our great gratitude to all the authors of the papers, reviewers, universities, faculties, business entities, national and international institutions and organizations that supported the conference. Without their help the organization and work of the conference would certainly not be at the level that its status deserves.

East Sarajevo, November 14th, 2022.

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Hong da hA

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PHASE-FIELD MODELING OF DAMAGE IN ALUMINUM ALLOY

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Abstract: Phase-Field Damage Model (PFDM) is a cutting-edge simulation tool for prediction of damage and crack evolution in materials. This paper shows simulation of AA5083-H321 ductile behavior using the modified PFDM coupled with a von Mises metal plasticity model. Uniaxial tensile tests at room temperature were performed on AA5083-H321 flat specimens in order to identify material parameters for numerical simulation and to verify the modified PFDM implemented into in-house software PAK. Comparison of the obtained results showed good agreement between experimental and simulation force-displacement responses.

Key words: Phase-field damage modeling, aluminum alloy, ductile fracture

1 INTRODUCTION

Phase-Field Damage Model (PFDM) coupled with von Mises metal plasticity was successfully used for simulation of S355 behavior in [1,2] by modifying the hardening function and the coupling variable. Two-intervals hardening function used in that research is then modified in [3], in order to simulate the aluminum alloy (AA) behavior. The improvements of coupled PFDM with plasticity are implemented into the in-house software PAK, developed at Faculty of Engineering, University of Kragujevac, Serbia. This paper shows the verification of implemented model by comparing the force-displacement diagrams obtained by numerical simulations and experimental tests. Sensitivity of the implemented model to the applied displacement increment size was also studied. Three AA5083-H321 flat specimens were investigated by static uniaxial tension tests at room temperature in order to use the representative specimen's recorded results to identify material parameters for numerical simulation. Comparison of results obtained by experiment and numerical simulations showed a

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good match and implemented model was successfully verified.

2 PHASE-FIELD DAMAGE MODEL COUPLED WITH PLASTICITY

Degradation function g(d) for PFDM is proposed by Ambati et al. [4,5] as

$$g(d) = (1-d)^{2p}$$
, (1)

where p represents a variable that couples PFDM and von Mises metal plasticity model. Authors of this paper modified the coupling variable in a way that its value is p=0 until the equivalent plastic strain reaches the critical value, i.e. $\frac{\overline{\mathcal{E}_p}}{\overline{\mathcal{E}_p^{crit}}} < 1$, because the material is considered to be undamaged in that case, and the value of coupling variable is $p=\frac{\overline{\mathcal{E}_p}}{\overline{\mathcal{E}_p^{crit}}}-1$ in case that $\frac{\overline{\mathcal{E}_p}}{\overline{\mathcal{E}_p^{crit}}} \ge 1$. Dependence of modified coupling variable on equivalent plastic strain is shown as continuous line in Figure 1, and the dashed line represents the value of coupling variable defined by Ambati et al. in [4].

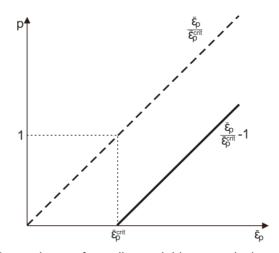


Figure 1. Dependence of coupling variable on equivalent plastic strain

In order to simulate behavior of aluminum alloy, that exhibits linear hardening after yielding occurs, it was necessary to modify the two-intervals hardening function used in [2] to describe the idealized response as continuous line in Figure 2. In the first interval, when $\bar{\varepsilon}_p < \bar{\varepsilon}_{p0}$, the yield stress can be defined by the linear hardening function parameter H_0 as

$$\sigma_{v} = \sigma_{vv} + H_{0} \overline{\varepsilon}_{p} . \tag{2}$$

The second interval starts when $\overline{\varepsilon}_p \geq \overline{\varepsilon}_{p0}$ and the nonlinear increase of the stress can be defined by Simo hardening function as

$$\sigma_{y} = \sigma_{y0} + (\sigma_{y0,\infty} - \sigma_{y0}) (1 - e^{-n(\overline{\varepsilon}_{p} - \overline{\varepsilon}_{p0})}) + H(\overline{\varepsilon}_{p} - \overline{\varepsilon}_{p0}),$$
(3)

where $\sigma_{y_0} = \sigma_{y_0} + H_0 \overline{\varepsilon}_{p_0}$. The dashed line in Figure 2 represents the theoretical influence of modified PFDM coupled with von Mises metal plasticity model. More details and stress integration algorithm for von Mises large strain plasticity are given in [1-3].

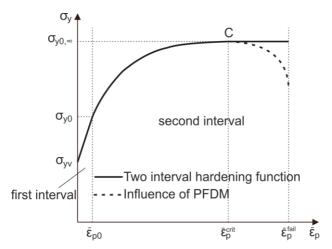


Figure 2. Idealized stress-strain response of AA5083

3 VERIFICATION OF MODIFIED PFDM

Three AA5083-H321 flat specimens, shown in Figure 3(a), were investigated at the Centre for Software Engineering and Dynamical Testing, Faculty of Engineering, University of Kragujevac, Serbia. Static uniaxial tensile tests were carried out at room temperature with a stroke control rate of 3 mm/min. Gauge length of the used extensometer MFA25 is 50 mm. Recorded force-displacement responses are shown in Figure 3(b). Fracture occurred within the gauge length only in case of a specimen wirh label 26, so those results are chosen as representative for verification of modified PFDM.

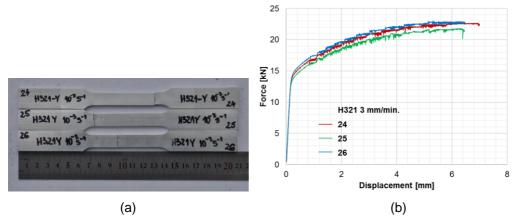


Figure 3. (a) AA5083-H321 specimens after uniaxial tensile tests; (b) recorded forcedisplacement response for AA5083-H321 specimens

Material parameters for PFDM simulation are obtained from real stress-real

strain curve of the specimen 26 and by calibration using the least squares method. Obtained values are given in Table 1, where E is Young's modulus, v is Poisson's ratio, H is hardening modulus, G_V is critical fracture release rate per unit volume, n is hardening exponent and I_c is characteristic length-scale parameter.

Table 1. Material parameters used for PFDM simulation

E [MPa]	<i>v</i> [-]	σ _{yv} [MPa]	<i>σ_{y0,∞}</i> [MPa]	H [MPa]	<i>H</i> ₀ [MPa]	G√ [MPa]	n [-]	I _c [mm]	$\overline{\mathcal{E}}_{P}^{crit}$ [-]	$\overline{\mathcal{E}}_{P0}$ [-]
70150	0.33	200.6	412.89	146.17	19817	2.55	20.3	0.01	0.11	0.0033

Model used for FEM simulation was 1/8 of the gauge section of tested specimen because of the three symmetry planes. Geometrical imperfection was prescribed as a 0.01% linear decrease of width and thickness where occurrence of necking is expected [3]. Four different displacement increments were applied to the top surface nodes of the FE model in order to investigate the sensitivity of the implemented method to the size of the displacement increment and results are shown in Figure 4.

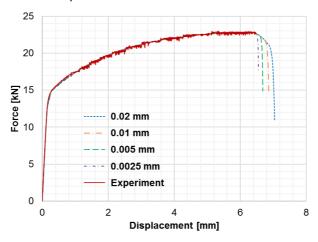


Figure 4. Force-displacement diagrams obtained for different displacement increments

The force-displacement response in softening zone is different for various displacement increments, so the part after the fracture point shouldn't be analyzed using this approach. Comparison of force-displacement diagrams obtained experimentally and by numerical simulations is shown in Figure 5. Two different FEM simulations with displacement increment of 0.0025mm were performed – by von Mises plasticity model ("Plasticity") and by PFDM coupled with plasticity ("PFDM + plasticity"), and the latter successfully reproduced the experimentally recorded response.

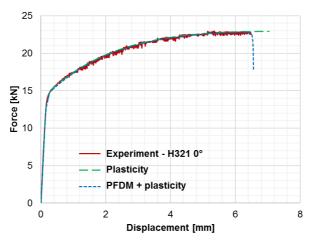


Figure 5. Force-displacement response of the numerical simulations and experiment

Figure 6(a) shows simulation results for the equivalent plastic strain field obtained by "pure" plasticity model and results obtained by PFDM coupled with plasticity are shown in Figure 6(b). It can be noticed that damage field, shown in Figure 6(c), has a big influence on localization of plastic strains and it can be concluded that the fracture process in material is caused by the occurrence of damage. Both equivalent plastic strain field and damage field, obtained by PFDM + plasticity simulation, are localized in the fracture zone of the experimentally tested specimen.

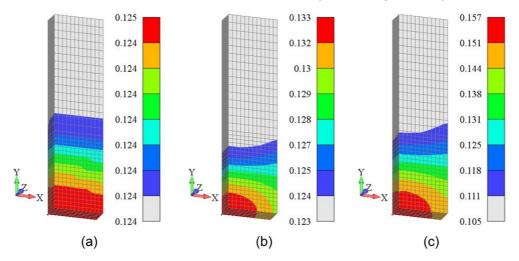


Figure 6. Simulation results: (a) effective plastic strain field – Plasticity; (b) effective plastic strain field – PFDM + plasticity; (c) Damage field – PFDM + plasticity

4 CONCLUSIONS

Authors previously verified [1,2] that PFDM coupled with von Mises metal plasticity, implemented into in-house software PAK, can successfully simulate behavior of steel structures. This paper shows three AA5083-H321 flat specimens that were investigated by static uniaxial tension tests at room temperature and the two-intervals hardening function that was modified in order to simulate the recorded response of

AA5083-H321 by using PFDM coupled with plasticity. Experimentally obtained force-displacement diagram is compared to diagrams obtained by two different FEM simulations - von Mises plasticity model and by PFDM coupled with plasticity and a good match between force-displacement diagrams is observed. Comparison of the damage field and the equivalent plastic strain field obtained by PFDM coupled with plasticity showed that the cause of the fracture of the specimen is the occurrence of damage. This and previous papers [1-3] show that implemented modified PFDM coupled with von Mises plasticity can be used to simulate the experimental response of various types of metallic materials with minimal modifications of the hardening function.

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