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Synthetic, Crystallographic, and Computational Study of Copper(II) Complexes of Ethylenediaminetetracarboxylate Ligands

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1. SUBMISSION DETAILS

_publ_contact_author_name # Name of author for correspondence

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Drs. A. Meetsma

;

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3. TITLE AND AUTHOR LIST

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The loop structure below should contain the names and addresses of all
authors, in the required order of publication. Repeat as necessary.

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; # author related footnote
;
; # Address of this author
;
'Meetsma, Auke'
;
? # author related footnote
;
;
Crystal Structure Center, Chemical Physics,
Zernike Institute for Advanced Materials,
University of Groningen,
Nijenborgh 4,
NL-9747 AG Groningen, The Netherlands.
;

```

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4. TEXT

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Insert blank lines between paragraphs

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;

The hydrogen atoms were generated by geometrical considerations, constrained to idealized geometries, and allowed to ride on the carrier atom with an isotropic displacement parameter related to the equivalent displacement parameter of their carrier atoms, with $U_{\text{iso}}(\text{H}) = 1.2U_{\text{eq}}(\text{C})$ or $1.5U_{\text{eq}}(\text{methyl C})$.

The methyl-groups were refined as rigid groups, which were allowed to rotate freely.

Assigned values of bond distances for secondary $\text{C-H}_{2} = 0.99 \text{ \AA}$,

The hydrogen atoms of the O-H bonds were leave free to a target value of and their isotropic displacement parameters (IDPs) were set to 1.5 times the U_{eq} value of their parent atom.

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;

Beurskens, P.T., Beurskens, G., Gelder, R. de, Garcia-Granda, S. Gould, R.O., Israel, & Smits, J.M.M. (1999). The <i>DIRDIF99</i> program system, Technical Report of the Crystallography Laboratory, University of Nijmegen, The Netherlands.

Bruker, (2001). <i>SMART</i>, SAINTPLUS and <i>XPREP</i>. Software Reference Manual Bruker AXS Inc. Madison, Wisconsin, USA.

Sheldrick, G. M. (1997). <i>SHELXL97</i>. Program for Crystal Structure Refinement. University of G"ottingen, Germany.

Spek, A. L. (2003). <i>J. Appl. Cryst.</i> **36**, 7--13.

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Fig. 1. Perspective PLUTO drawings of the molecule illustrating the

configuration and the adopted numbering scheme.

Fig. 2. Molecular packing viewed down unit cell axes.

Fig. 3. Perspective ORTEP drawing of the title compound.
Displacement ellipsoids for non-H atoms are represented at the 50% probability level.

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5. CHEMICAL DATA

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_chemical_formula_moiety

'C13 H18 Ba Cu N2 O8, 8(H2 O)'

Ex: 'C12 H16 N2 O6, H2 O' and '(Cd 2+)3, (C6 N6 Cr 3-)2, 2(H2 O)'

_chemical_formula_structural ?

_chemical_formula_sum

'C13 H34 Ba Cu N2 O16'

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_atom_type_description

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Cu Cu 0.3201 1.2651

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Ba Ba -0.3244 2.2819

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C C 0.0033 0.0016

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6. CRYSTAL DATA

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loop_

_symmetry_equiv_pos_site_id

_symmetry_equiv_pos_as_xyz

1 x, y, z

2 -x, -y, -z

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_cell_length_b 11.8362(5)
_cell_length_c 11.9806(5)
_cell_angle_alpha 101.056(1)
_cell_angle_beta 108.737(1)
_cell_angle_gamma 95.195(1)
_cell_volume 1180.29(9)
_cell_formula_units_Z 2

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_cell_measurement_reflns_used 9337
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_cell_special_details

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The final unit cell was obtained from the xyz centroids of 9337 reflections after integration using the SAINTPLUS software package (Bruker, 2000).

Reduced cell calculations did not indicate any higher metric lattice symmetry and examination of the final atomic coordinates of the structure did not yield extra symmetry elements (Spek, 1988; Le Page 1987, 1988)

;

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;

CCD area-detector

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Bruker Smart Apex; CCD area detector

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_diffrn_measurement_method '\f and \w scans'

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Crystal into the cold nitrogen stream of the low-temperature unit

```

(KRYOFLEX, (Bruker, 2000)).
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? ? ?

# number of measured reflections (redundant set)
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_diffrn_reflns_theta_min               2.24
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_diffrn_measured_fraction_theta_max   0.960
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_diffrn_reflns_reduction_process
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Intensity data were corrected for Lorentz and polarization
effects, decay and absorption and reduced to  $F_o^2$ 
using SAINT (Bruker, 2000) and SADABS (Sheldrick, 2001)
;

# number of unique reflections
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DIRDIF-99 (Beurskens et al., 1999)
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PLUTO (Meetsma, 2006)
PLATON (Spek, 2003)
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# 8. REFINEMENT DATA

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Refinement of F^2 against ALL reflections. The weighted R-factor wR and goodness of fit S are based on F^2 , conventional R-factors R are based on F, with F set to zero for negative F^2 . The threshold expression of $F^2 > 2\sigma(F^2)$ is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on F^2 are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger.

;

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Cu Cu Uani 0.80510(3) 0.21778(2) 0.29180(2) 1.0 0.0113(1) . . . .
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O1	O	Uani	0.98645(19)	0.13973(14)	0.29569(14)	1.0	0.0161(4)
O2	O	Uani	1.1839(2)	0.08752(15)	0.23935(15)	1.0	0.0192(5)
O3	O	Uani	0.6241(2)	0.03366(14)	0.15797(15)	1.0	0.0190(5)
O4	O	Uani	0.7664(2)	-0.10408(15)	0.12021(16)	1.0	0.0249(6)
O5	O	Uani	0.98434(19)	0.35989(14)	0.44662(14)	1.0	0.0157(4)
O6	O	Uani	1.0149(2)	0.35919(16)	0.63848(15)	1.0	0.0206(5)
O7	O	Uani	0.74574(19)	0.14838(13)	0.41525(14)	1.0	0.0145(4)
O8	O	Uani	0.53672(19)	0.10704(14)	0.46801(14)	1.0	0.0152(5)
O24	O	Uani	1.2401(2)	-0.12805(16)	0.26496(16)	1.0	0.0194(5)
O25	O	Uani	1.2722(2)	0.28326(15)	0.51929(16)	1.0	0.0183(5)
O27	O	Uani	1.4459(2)	0.11633(15)	0.71288(16)	1.0	0.0163(5)
O28	O	Uani	1.0653(2)	0.11434(15)	0.63277(15)	1.0	0.0162(5)
N1	N	Uani	0.7949(3)	0.26769(18)	0.13729(18)	1.0	0.0200(6)
N2	N	Uani	0.6307(2)	0.30989(18)	0.30142(18)	1.0	0.0185(6)
C1	C	Uani	1.0790(3)	0.1491(2)	0.2359(2)	1.0	0.0164(6)
C2	C	Uani	1.0722(3)	0.2382(2)	0.1575(2)	1.0	0.0230(7)
C3	C	Uani	0.9554(3)	0.3222(2)	0.1524(2)	1.0	0.0225(7)
C4	C	Uani	0.7197(3)	0.1747(2)	0.0220(2)	1.0	0.0213(7)
C5	C	Uani	0.7592(3)	0.0513(2)	0.0190(2)	1.0	0.0196(6)
C6	C	Uani	0.7131(3)	-0.0109(2)	0.1063(2)	1.0	0.0182(6)
C7	C	Uani	0.6929(3)	0.3635(2)	0.1349(2)	1.0	0.0203(7)
C8	C	Uani	0.5606(3)	0.3303(2)	0.1783(2)	1.0	0.0214(7)
C9	C	Uani	0.6870(3)	0.4247(2)	0.3930(2)	1.0	0.0193(6)
C10	C	Uani	0.7775(3)	0.4146(2)	0.5203(2)	1.0	0.0175(6)
C11	C	Uani	0.9370(3)	0.37473(19)	0.5362(2)	1.0	0.0159(6)
C12	C	Uani	0.5171(3)	0.2333(2)	0.3331(2)	1.0	0.0185(6)
C13	C	Uani	0.6047(3)	0.15829(19)	0.4123(2)	1.0	0.0143(6)
O21	O	Uani	0.7659(2)	0.66118(17)	0.06159(17)	1.0	0.0232(5)
O22	O	Uani	0.0769(2)	0.65073(16)	0.17716(17)	1.0	0.0210(5)
O23	O	Uani	0.5838(2)	0.65497(17)	0.21733(18)	1.0	0.0235(6)
O26	O	Uani	0.2937(3)	0.51643(19)	0.1445(2)	1.0	0.0317(6)
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H2'	H	Uiso	1.05102	0.19405	0.07340	1.0	0.0276
H3	H	Uiso	0.99552	0.38445	0.22805	1.0	0.0270
H3'	H	Uiso	0.94890	0.35952	0.08411	1.0	0.0270
H4	H	Uiso	0.74767	0.20228	-0.04275	1.0	0.0257
H4'	H	Uiso	0.60396	0.16887	0.00002	1.0	0.0257
H5	H	Uiso	0.70587	0.00304	-0.06441	1.0	0.0235
H5'	H	Uiso	0.87417	0.05562	0.03726	1.0	0.0235
H7	H	Uiso	0.75789	0.43811	0.18776	1.0	0.0244
H7'	H	Uiso	0.64913	0.37435	0.05126	1.0	0.0244
H8	H	Uiso	0.49690	0.39369	0.18078	1.0	0.0256
H8'	H	Uiso	0.49103	0.25861	0.12246	1.0	0.0256
H9	H	Uiso	0.59474	0.46272	0.39452	1.0	0.0232
H9'	H	Uiso	0.75558	0.47573	0.36688	1.0	0.0232
H10	H	Uiso	0.71173	0.35878	0.54374	1.0	0.0210
H10'	H	Uiso	0.79480	0.49156	0.57660	1.0	0.0210
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H12'	H	Uiso	0.46044	0.28218	0.37655	1.0	0.0222
H24	H	Uiso	1.184(4)	-0.200(3)	0.236(3)	1.0	0.0291
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H25	H	Uiso	1.313(4)	0.306(3)	0.591(3)	1.0	0.0275
H25'	H	Uiso	1.182(4)	0.308(3)	0.499(3)	1.0	0.0275
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H27'	H	Uiso	1.518(4)	0.121(3)	0.715(3)	1.0	0.0244
H28	H	Uiso	1.113(4)	0.112(3)	0.700(3)	1.0	0.0243
H28'	H	Uiso	1.059(4)	0.179(3)	0.638(3)	1.0	0.0243
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H21'	H	Uiso	0.761(4)	0.727(3)	0.068(3)	1.0	0.0347
H22	H	Uiso	0.125(4)	0.615(3)	0.165(3)	1.0	0.0315
H22'	H	Uiso	0.061(4)	0.639(3)	0.240(3)	1.0	0.0315
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H23'	H	Uiso	0.567(5)	0.708(3)	0.221(3)	1.0	0.0352
H26	H	Uiso	0.265(5)	0.467(4)	0.083(4)	1.0	0.0475
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O5 0.0153(8) 0.0131(7) 0.0166(8) 0.0023(6) 0.0035(6) 0.0019(6)
O6 0.0192(8) 0.0257(9) 0.0172(8) 0.0058(7) 0.0054(7) 0.0070(7)
O7 0.0156(8) 0.0126(7) 0.0172(8) 0.0028(6) 0.0092(6) 0.0006(6)
O8 0.0152(8) 0.0148(8) 0.0201(8) 0.0078(6) 0.0093(6) 0.0045(6)
O24 0.0240(9) 0.0145(8) 0.0206(8) 0.0045(7) 0.0081(7) 0.0052(7)
O25 0.0177(9) 0.0159(8) 0.0197(8) 0.0023(7) 0.0046(7) 0.0058(7)
O27 0.0153(8) 0.0170(8) 0.0186(8) 0.0057(6) 0.0077(7) 0.0027(7)
O28 0.0170(8) 0.0157(8) 0.0161(8) 0.0039(7) 0.0054(6) 0.0046(7)
N1 0.0254(11) 0.0181(10) 0.0146(9) 0.0050(8) 0.0052(8) -0.0012(8)
N2 0.0172(10) 0.0158(9) 0.0196(10) 0.0035(8) 0.0021(8) 0.0051(8)
C1 0.0180(11) 0.0167(11) 0.0129(10) 0.0021(8) 0.0037(8) 0.0040(9)
C2 0.0267(13) 0.0207(12) 0.0221(12) 0.0091(10) 0.0065(10) 0.0050(10)
C3 0.0261(13) 0.0194(12) 0.0228(12) 0.0079(10) 0.0079(10) 0.0035(10)
C4 0.0314(14) 0.0188(11) 0.0113(10) 0.0041(9) 0.0048(9) -0.0001(10)
C5 0.0258(12) 0.0179(11) 0.0131(10) 0.0029(8) 0.0053(9) 0.0009(10)
C6 0.0217(12) 0.0148(11) 0.0127(10) 0.0019(8) 0.0009(9) -0.0021(9)
C7 0.0232(12) 0.0168(11) 0.0208(11) 0.0119(9) 0.0031(9) 0.0034(9)
C8 0.0219(12) 0.0199(12) 0.0218(12) 0.0074(9) 0.0050(10) 0.0048(10)
C9 0.0184(11) 0.0132(11) 0.0222(11) 0.0014(9) 0.0020(9) 0.0066(9)
C10 0.0154(11) 0.0137(10) 0.0202(11) 0.0003(8) 0.0036(9) 0.0037(9)
C11 0.0149(11) 0.0104(10) 0.0205(11) 0.0025(8) 0.0043(9) 0.0024(8)
C12 0.0193(11) 0.0129(10) 0.0218(11) 0.0069(9) 0.0036(9) 0.0021(9)
C13 0.0185(11) 0.0088(9) 0.0143(10) 0.0008(8) 0.0054(8) 0.0011(8)
O21 0.0219(9) 0.0184(9) 0.0252(9) 0.0011(7) 0.0047(7) 0.0049(8)
O22 0.0225(9) 0.0205(9) 0.0218(9) 0.0037(7) 0.0098(7) 0.0068(7)
O23 0.0258(10) 0.0172(9) 0.0277(10) 0.0021(8) 0.0107(8) 0.0061(8)
O26 0.0264(11) 0.0249(11) 0.0343(11) -0.0079(9) 0.0068(9) 0.0031(8)

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# 10. MOLECULAR GEOMETRY
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;
Bond distances, angles etc. have been calculated using the
rounded fractional coordinates. All su's are estimated
from the variances of the (full) variance-covariance matrix.
The cell esds are taken into account in the estimation of
distances, angles and torsion angles
;
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loop_
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_geom_bond_atom_site_label_2
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Ba O1 3.0481(17) . . yes
Ba O2 2.8337(17) . . yes
Ba O24 2.8828(18) . . yes
Ba O25 2.7744(18) . . yes

```

Ba	O27	2.8170(18)	.	.	yes
Ba	O28	2.9044(18)	.	.	yes
Ba	O8	2.7778(18)	.	1_655	yes
Ba	O7	2.8321(16)	.	2_756	yes
Ba	O8	2.8346(18)	.	2_756	yes
Ba	O28	2.9135(19)	.	2_756	yes
Cu	O1	1.9515(18)	.	.	yes
Cu	O3	2.5177(17)	.	.	yes
Cu	O5	2.2991(17)	.	.	yes
Cu	O7	2.0126(16)	.	.	yes
Cu	N1	2.026(2)	.	.	yes
Cu	N2	2.022(2)	.	.	yes
O1	C1	1.277(3)	.	.	yes
O2	C1	1.246(3)	.	.	yes
O3	C6	1.260(3)	.	.	yes
O4	C6	1.262(3)	.	.	yes
O5	C11	1.267(3)	.	.	yes
O6	C11	1.261(3)	.	.	yes
O7	C13	1.286(3)	.	.	yes
O8	C13	1.244(3)	.	.	yes
O24	H24'	0.73(4)	.	.	no
O24	H24	0.89(4)	.	.	no
O25	H25'	0.87(4)	.	.	no
O25	H25	0.80(3)	.	.	no
O27	H27	0.77(4)	.	.	no
O27	H27'	0.64(4)	.	.	no
O28	H28	0.79(3)	.	.	no
O28	H28'	0.77(4)	.	.	no
O21	H21	0.83(4)	.	.	no
O21	H21'	0.78(4)	.	.	no
O22	H22	0.66(4)	.	.	no
O22	H22'	0.85(3)	.	.	no
O23	H23'	0.66(4)	.	.	no
O23	H23	0.77(4)	.	.	no
O26	H26'	0.67(5)	.	.	no
O26	H26	0.80(4)	.	.	no
N1	C7	1.526(4)	.	.	yes
N1	C3	1.479(4)	.	.	yes
N1	C4	1.504(3)	.	.	yes
N2	C9	1.501(3)	.	.	yes
N2	C12	1.498(3)	.	.	yes
N2	C8	1.483(3)	.	.	yes
C1	C2	1.534(3)	.	.	no
C2	C3	1.513(4)	.	.	no
C4	C5	1.532(3)	.	.	no
C5	C6	1.527(3)	.	.	no
C7	C8	1.504(4)	.	.	no
C9	C10	1.516(3)	.	.	no
C10	C11	1.529(4)	.	.	no
C12	C13	1.512(3)	.	.	no
C2	H2'	0.99	.	.	no
C2	H2	0.99	.	.	no
C3	H3	0.99	.	.	no
C3	H3'	0.99	.	.	no
C4	H4	0.99	.	.	no
C4	H4'	0.99	.	.	no
C5	H5	0.99	.	.	no
C5	H5'	0.99	.	.	no
C7	H7	0.99	.	.	no
C7	H7'	0.99	.	.	no
C8	H8'	0.99	.	.	no
C8	H8	0.99	.	.	no
C9	H9'	0.99	.	.	no
C9	H9	0.99	.	.	no
C10	H10	0.99	.	.	no
C10	H10'	0.99	.	.	no

C12	H12	0.99	.	.		no
C12	H12'	0.99	.	.		no
loop_						
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_geom_angle_site_symmetry_2						
_geom_angle_site_symmetry_3						
_geom_angle_publ_flag						
01	Ba	O2	43.87(5)	.	.	yes
01	Ba	O24	87.72(5)	.	.	yes
01	Ba	O25	64.79(5)	.	.	yes
01	Ba	O27	137.07(5)	.	.	yes
01	Ba	O28	82.97(5)	.	.	yes
01	Ba	O8	112.16(5)	.	1_655	yes
01	Ba	O7	138.06(5)	.	2_756	yes
01	Ba	O8	154.10(4)	.	2_756	yes
01	Ba	O28	67.53(5)	.	2_756	yes
02	Ba	O24	56.41(5)	.	.	yes
02	Ba	O25	77.09(5)	.	.	yes
02	Ba	O27	141.16(5)	.	.	yes
02	Ba	O28	126.36(5)	.	.	yes
02	Ba	O8	75.49(5)	.	1_655	yes
02	Ba	O7	140.21(5)	.	2_756	yes
02	Ba	O8	113.49(5)	.	2_756	yes
02	Ba	O28	87.59(5)	.	2_756	yes
024	Ba	O25	131.25(5)	.	.	yes
024	Ba	O27	132.80(5)	.	.	yes
024	Ba	O28	146.04(5)	.	.	yes
08	Ba	O24	78.19(5)	1_655	.	yes
07	Ba	O24	84.61(5)	2_756	.	yes
08	Ba	O24	66.55(5)	2_756	.	yes
024	Ba	O28	71.26(5)	.	2_756	yes
025	Ba	O27	75.59(5)	.	.	yes
025	Ba	O28	72.84(5)	.	.	yes
08	Ba	O25	76.66(5)	1_655	.	yes
07	Ba	O25	142.65(5)	2_756	.	yes
08	Ba	O25	130.39(5)	2_756	.	yes
025	Ba	O28	124.61(5)	.	2_756	yes
027	Ba	O28	69.74(5)	.	.	yes
08	Ba	O27	71.73(5)	1_655	.	yes
07	Ba	O27	70.58(5)	2_756	.	yes
08	Ba	O27	67.31(5)	2_756	.	yes
027	Ba	O28	130.85(5)	.	2_756	yes
08	Ba	O28	135.43(5)	1_655	.	yes
07	Ba	O28	80.91(5)	2_756	.	yes
08	Ba	O28	119.91(5)	2_756	.	yes
028	Ba	O28	75.01(5)	.	2_756	yes
07	Ba	O8	106.45(5)	2_756	1_655	yes
08	Ba	O8	61.43(5)	1_655	2_756	yes
08	Ba	O28	149.45(5)	1_655	2_756	yes
07	Ba	O8	46.29(5)	2_756	2_756	yes
07	Ba	O28	70.96(5)	2_756	2_756	yes
08	Ba	O28	104.66(5)	2_756	2_756	yes
01	Cu	O3	89.66(7)	.	.	yes
01	Cu	O5	84.82(7)	.	.	yes
01	Cu	O7	97.12(7)	.	.	yes
01	Cu	N1	93.38(9)	.	.	yes
01	Cu	N2	174.68(8)	.	.	yes
03	Cu	O5	166.67(6)	.	.	yes
03	Cu	O7	79.26(6)	.	.	yes
03	Cu	N1	86.79(7)	.	.	yes
03	Cu	N2	95.42(7)	.	.	yes

O5	Cu	O7	89.37(6)	.	.	.	yes
O5	Cu	N1	105.62(8)	.	.	.	yes
O5	Cu	N2	89.88(7)	.	.	.	yes
O7	Cu	N1	162.44(9)	.	.	.	yes
O7	Cu	N2	82.31(8)	.	.	.	yes
N1	Cu	N2	88.50(10)	.	.	.	yes
Ba	O1	Cu	139.32(7)	.	.	.	yes
Ba	O1	C1	88.71(14)	.	.	.	yes
Cu	O1	C1	128.14(16)	.	.	.	yes
Ba	O2	C1	99.50(14)	.	.	.	yes
Cu	O3	C6	100.24(15)	.	.	.	yes
Cu	O5	C11	108.27(15)	.	.	.	yes
Cu	O7	C13	113.09(14)	.	.	.	yes
Ba	O7	Cu	145.23(8)	2_756	.	.	yes
Ba	O7	C13	94.14(13)	2_756	.	.	yes
Ba	O8	C13	140.90(16)	1_455	.	.	yes
Ba	O8	C13	95.04(15)	2_756	.	.	yes
Ba	O8	Ba	118.57(6)	1_455	.	2_756	yes
Ba	O28	Ba	104.99(5)	.	.	2_756	yes
Ba	O24	H24'	81(3)	.	.	.	no
H24	O24	H24'	115(4)	.	.	.	no
Ba	O24	H24	126(2)	.	.	.	no
H25	O25	H25'	107(4)	.	.	.	no
Ba	O25	H25	106(3)	.	.	.	no
Ba	O25	H25'	112(2)	.	.	.	no
Ba	O27	H27	112(3)	.	.	.	no
H27	O27	H27'	114(4)	.	.	.	no
Ba	O27	H27'	111(3)	.	.	.	no
Ba	O28	H28	111(3)	.	.	.	no
Ba	O28	H28'	114(3)	2_756	.	.	no
Ba	O28	H28	113(3)	2_756	.	.	no
Ba	O28	H28'	110(3)	.	.	.	no
H28	O28	H28'	103(4)	.	.	.	no
H21	O21	H21'	105(4)	.	.	.	no
H22	O22	H22'	108(4)	.	.	.	no
H23	O23	H23'	108(5)	.	.	.	no
H26	O26	H26'	113(5)	.	.	.	no
Cu	N1	C4	115.60(16)	.	.	.	yes
Cu	N1	C7	103.51(15)	.	.	.	yes
C3	N1	C7	107.71(19)	.	.	.	yes
C4	N1	C7	108.3(2)	.	.	.	yes
C3	N1	C4	113.2(2)	.	.	.	yes
Cu	N1	C3	107.86(15)	.	.	.	yes
Cu	N2	C12	105.94(15)	.	.	.	yes
C8	N2	C9	109.63(19)	.	.	.	yes
C8	N2	C12	112.14(19)	.	.	.	yes
C9	N2	C12	110.32(18)	.	.	.	yes
Cu	N2	C8	104.97(15)	.	.	.	yes
Cu	N2	C9	113.75(15)	.	.	.	yes
O1	C1	O2	122.0(2)	.	.	.	yes
O2	C1	C2	115.2(2)	.	.	.	yes
O1	C1	C2	122.8(2)	.	.	.	yes
C1	C2	C3	119.7(2)	.	.	.	no
N1	C3	C2	114.3(2)	.	.	.	yes
N1	C4	C5	119.0(2)	.	.	.	yes
C4	C5	C6	115.8(2)	.	.	.	no
O3	C6	O4	125.0(2)	.	.	.	yes
O3	C6	C5	117.9(2)	.	.	.	yes
O4	C6	C5	117.1(2)	.	.	.	yes
N1	C7	C8	109.6(2)	.	.	.	yes
N2	C8	C7	108.1(2)	.	.	.	yes
N2	C9	C10	113.9(2)	.	.	.	yes
C9	C10	C11	114.8(2)	.	.	.	no
O5	C11	O6	123.6(3)	.	.	.	yes
O5	C11	C10	118.5(2)	.	.	.	yes
O6	C11	C10	117.9(2)	.	.	.	yes

N2	C12	C13	110.0(2)	.	.	.	yes
O7	C13	C12	117.4(2)	.	.	.	yes
O8	C13	C12	119.2(2)	.	.	.	yes
O7	C13	O8	123.4(2)	.	.	.	yes
C3	C2	H2'	107	.	.	.	no
C1	C2	H2	107	.	.	.	no
C1	C2	H2'	107	.	.	.	no
H2	C2	H2'	107	.	.	.	no
C3	C2	H2	107	.	.	.	no
N1	C3	H3	109	.	.	.	no
N1	C3	H3'	109	.	.	.	no
C2	C3	H3	109	.	.	.	no
C2	C3	H3'	109	.	.	.	no
H3	C3	H3'	108	.	.	.	no
N1	C4	H4'	108	.	.	.	no
C5	C4	H4	108	.	.	.	no
C5	C4	H4'	108	.	.	.	no
N1	C4	H4	108	.	.	.	no
H4	C4	H4'	107	.	.	.	no
C6	C5	H5'	108	.	.	.	no
H5	C5	H5'	107	.	.	.	no
C4	C5	H5	108	.	.	.	no
C4	C5	H5'	108	.	.	.	no
C6	C5	H5	108	.	.	.	no
N1	C7	H7'	110	.	.	.	no
C8	C7	H7	110	.	.	.	no
N1	C7	H7	110	.	.	.	no
C8	C7	H7'	110	.	.	.	no
H7	C7	H7'	108	.	.	.	no
H8	C8	H8'	108	.	.	.	no
C7	C8	H8	110	.	.	.	no
C7	C8	H8'	110	.	.	.	no
N2	C8	H8	110	.	.	.	no
N2	C8	H8'	110	.	.	.	no
H9	C9	H9'	108	.	.	.	no
N2	C9	H9	109	.	.	.	no
N2	C9	H9'	109	.	.	.	no
C10	C9	H9	109	.	.	.	no
C10	C9	H9'	109	.	.	.	no
C9	C10	H10'	109	.	.	.	no
C11	C10	H10	109	.	.	.	no
C9	C10	H10	109	.	.	.	no
C11	C10	H10'	109	.	.	.	no
H10	C10	H10'	108	.	.	.	no
H12	C12	H12'	108	.	.	.	no
C13	C12	H12	110	.	.	.	no
C13	C12	H12'	110	.	.	.	no
N2	C12	H12	110	.	.	.	no
N2	C12	H12'	110	.	.	.	no

loop_

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_geom_torsion_publ_flag

O2	Ba	O1	Cu	-170.01(16)	.	.	.	no
O2	Ba	O1	C1	-12.87(13)	.	.	.	no
O24	Ba	O1	Cu	149.24(12)	.	.	.	no
O24	Ba	O1	C1	-53.62(13)	.	.	.	no
O25	Ba	O1	Cu	-72.34(12)	.	.	.	no

025	Ba	01	C1	84.81(14)	no
027	Ba	01	Cu	-47.88(15)	no
027	Ba	01	C1	109.26(14)	no
028	Ba	01	Cu	1.96(12)	no
028	Ba	01	C1	159.11(14)	no
08	Ba	01	Cu	-134.49(11)	1_655	.	.	.	no
08	Ba	01	C1	22.66(14)	1_655	.	.	.	no
07	Ba	01	Cu	69.91(14)	2_756	.	.	.	no
07	Ba	01	C1	-132.95(13)	2_756	.	.	.	no
08	Ba	01	Cu	155.59(10)	2_756	.	.	.	no
08	Ba	01	C1	-47.26(19)	2_756	.	.	.	no
028	Ba	01	Cu	78.60(12)	2_756	.	.	.	no
028	Ba	01	C1	-124.25(14)	2_756	.	.	.	no
01	Ba	02	C1	13.38(14)	no
024	Ba	02	C1	141.84(17)	no
025	Ba	02	C1	-53.53(15)	no
027	Ba	02	C1	-99.75(16)	no
028	Ba	02	C1	3.47(17)	no
08	Ba	02	C1	-132.85(16)	1_655	.	.	.	no
07	Ba	02	C1	128.73(15)	2_756	.	.	.	no
08	Ba	02	C1	177.77(14)	2_756	.	.	.	no
028	Ba	02	C1	72.83(15)	2_756	.	.	.	no
01	Ba	028	Ba	68.55(5)	.	.	.	2_756	no
02	Ba	028	Ba	75.45(7)	.	.	.	2_756	no
024	Ba	028	Ba	-6.68(12)	.	.	.	2_756	no
025	Ba	028	Ba	134.27(7)	.	.	.	2_756	no
027	Ba	028	Ba	-145.15(7)	.	.	.	2_756	no
08	Ba	028	Ba	-176.85(5)	1_655	.	.	2_756	no
07	Ba	028	Ba	-72.60(6)	2_756	.	.	2_756	no
08	Ba	028	Ba	-98.52(6)	2_756	.	.	2_756	no
028	Ba	028	Ba	0.00(4)	2_756	.	.	2_756	no
01	Ba	08	C13	-6.2(2)	.	.	1_655	1_655	no
02	Ba	08	C13	18.4(2)	.	.	1_655	1_655	no
024	Ba	08	C13	76.4(2)	.	.	1_655	1_655	no
025	Ba	08	C13	-61.5(2)	.	.	1_655	1_655	no
027	Ba	08	C13	-140.5(2)	.	.	1_655	1_655	no
028	Ba	08	C13	-109.2(2)	.	.	1_655	1_655	no
01	Ba	07	Cu	-68.80(15)	.	.	2_756	2_756	no
01	Ba	07	C13	148.67(12)	.	.	2_756	2_756	no
02	Ba	07	Cu	-138.37(12)	.	.	2_756	2_756	no
02	Ba	07	C13	79.10(15)	.	.	2_756	2_756	no
024	Ba	07	Cu	-149.31(14)	.	.	2_756	2_756	no
024	Ba	07	C13	68.16(13)	.	.	2_756	2_756	no
025	Ba	07	Cu	45.26(18)	.	.	2_756	2_756	no
025	Ba	07	C13	-97.27(14)	.	.	2_756	2_756	no
027	Ba	07	Cu	71.50(13)	.	.	2_756	2_756	no
027	Ba	07	C13	-71.04(13)	.	.	2_756	2_756	no
028	Ba	07	Cu	-0.12(13)	.	.	2_756	2_756	no
028	Ba	07	C13	-142.65(13)	.	.	2_756	2_756	no
01	Ba	08	C13	-118.70(15)	.	.	2_756	2_756	no
02	Ba	08	C13	-143.97(13)	.	.	2_756	2_756	no
024	Ba	08	C13	-111.77(14)	.	.	2_756	2_756	no
025	Ba	08	C13	123.17(13)	.	.	2_756	2_756	no
027	Ba	08	C13	78.40(13)	.	.	2_756	2_756	no
028	Ba	08	C13	30.74(15)	.	.	2_756	2_756	no
01	Ba	028	Ba	-88.49(6)	.	.	2_756	2_756	no
02	Ba	028	Ba	-128.72(6)	.	.	2_756	2_756	no
024	Ba	028	Ba	176.07(7)	.	.	2_756	2_756	no
025	Ba	028	Ba	-56.22(8)	.	.	2_756	2_756	no
027	Ba	028	Ba	45.13(9)	.	.	2_756	2_756	no
028	Ba	028	Ba	0.00(6)	.	.	2_756	2_756	no
03	Cu	01	Ba	-107.87(11)	no
03	Cu	01	C1	101.72(19)	no
05	Cu	01	Ba	59.98(11)	no
05	Cu	01	C1	-90.44(19)	no
07	Cu	01	Ba	-28.73(12)	no

O7	Cu	O1	C1	-179.15(19)	no
N1	Cu	O1	Ba	165.37(12)	no
N1	Cu	O1	C1	15.0(2)	no
O1	Cu	O3	C6	-27.69(14)	no
O7	Cu	O3	C6	-125.00(15)	no
N1	Cu	O3	C6	65.71(16)	no
N2	Cu	O3	C6	153.90(15)	no
O1	Cu	O5	C11	-124.50(16)	no
O7	Cu	O5	C11	-27.29(16)	no
N1	Cu	O5	C11	143.43(16)	no
N2	Cu	O5	C11	55.02(16)	no
O1	Cu	O7	C13	-162.92(15)	no
O1	Cu	O7	Ba	-24.19(14)	.	.	.	2_756	no
O3	Cu	O7	C13	-74.62(15)	no
O3	Cu	O7	Ba	64.11(13)	.	.	.	2_756	no
O5	Cu	O7	C13	112.38(15)	no
O5	Cu	O7	Ba	-108.89(13)	.	.	.	2_756	no
N2	Cu	O7	C13	22.42(15)	no
N2	Cu	O7	Ba	161.15(14)	.	.	.	2_756	no
O1	Cu	N1	C3	-49.04(16)	no
O1	Cu	N1	C4	78.7(2)	no
O1	Cu	N1	C7	-163.00(15)	no
O3	Cu	N1	C3	-138.51(16)	no
O3	Cu	N1	C4	-10.7(2)	no
O3	Cu	N1	C7	107.53(15)	no
O5	Cu	N1	C3	36.52(17)	no
O5	Cu	N1	C4	164.30(18)	no
O5	Cu	N1	C7	-77.44(16)	no
N2	Cu	N1	C3	125.97(16)	no
N2	Cu	N1	C4	-106.3(2)	no
N2	Cu	N1	C7	12.02(16)	no
O3	Cu	N2	C8	-69.85(15)	no
O3	Cu	N2	C9	170.31(15)	no
O3	Cu	N2	C12	48.96(14)	no
O5	Cu	N2	C8	122.40(15)	no
O5	Cu	N2	C9	2.56(15)	no
O5	Cu	N2	C12	-118.78(14)	no
O7	Cu	N2	C8	-148.22(15)	no
O7	Cu	N2	C9	91.94(16)	no
O7	Cu	N2	C12	-29.40(13)	no
N1	Cu	N2	C8	16.78(16)	no
N1	Cu	N2	C9	-103.06(16)	no
N1	Cu	N2	C12	135.60(15)	no
Ba	O1	C1	O2	24.4(2)	no
Ba	O1	C1	C2	-154.1(2)	no
Cu	O1	C1	O2	-174.33(16)	no
Cu	O1	C1	C2	7.2(3)	no
Ba	O2	C1	O1	-26.8(2)	no
Ba	O2	C1	C2	151.79(16)	no
Cu	O3	C6	O4	113.4(2)	no
Cu	O3	C6	C5	-67.3(2)	no
Cu	O5	C11	O6	119.8(2)	no
Cu	O5	C11	C10	-60.7(2)	no
Cu	O7	C13	O8	169.20(18)	no
Cu	O7	C13	C12	-8.7(2)	no
Ba	O7	C13	O8	11.4(2)	2_756	.	.	.	no
Ba	O7	C13	C12	-166.51(17)	2_756	.	.	.	no
Ba	O8	C13	O7	-161.79(15)	1_455	.	.	.	no
Ba	O8	C13	C12	16.1(4)	1_455	.	.	.	no
Ba	O8	C13	O7	-11.4(2)	2_756	.	.	.	no
Ba	O8	C13	C12	166.47(18)	2_756	.	.	.	no
Cu	N1	C3	C2	68.4(2)	no
C4	N1	C3	C2	-60.7(3)	no
C7	N1	C3	C2	179.55(18)	no
Cu	N1	C4	C5	-42.3(3)	no
C3	N1	C4	C5	82.8(3)	no

C7	N1	C4	C5	-157.8(2)	no
Cu	N1	C7	C8	-39.3(2)	no
C3	N1	C7	C8	-153.39(18)	no
C4	N1	C7	C8	83.9(2)	no
Cu	N2	C8	C7	-42.9(2)	no
C9	N2	C8	C7	79.7(2)	no
C12	N2	C8	C7	-157.41(19)	no
Cu	N2	C9	C10	-56.2(3)	no
C8	N2	C9	C10	-173.4(2)	no
C12	N2	C9	C10	62.6(3)	no
Cu	N2	C12	C13	32.3(2)	no
C8	N2	C12	C13	146.27(19)	no
C9	N2	C12	C13	-91.2(2)	no
O1	C1	C2	C3	2.0(3)	no
O2	C1	C2	C3	-176.6(2)	no
C1	C2	C3	N1	-45.1(3)	no
N1	C4	C5	C6	62.0(3)	no
C4	C5	C6	O3	11.8(3)	no
C4	C5	C6	O4	-168.8(2)	no
N1	C7	C8	N2	57.0(2)	no
N2	C9	C10	C11	67.5(3)	no
C9	C10	C11	O5	3.8(3)	no
C9	C10	C11	O6	-176.7(2)	no
N2	C12	C13	O7	-16.7(3)	no
N2	C12	C13	O8	165.3(2)	no

loop_

_geom_hbond_atom_site_label_D

_geom_hbond_atom_site_label_H

_geom_hbond_atom_site_label_A

_geom_hbond_distance_DH

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_geom_hbond_angle_DHA

_geom_hbond_site_symmetry_A

_geom_hbond_publ_flag

#

#D	H	A	D - H	H...A	D...A	D - H...A	symm(A)		
#									
O21	H21	O22		0.83(4)	1.91(4)	2.742(3)	176(4)	1_655	yes
O21	H21'	O4		0.78(4)	1.97(4)	2.731(3)	168(3)	1_565	yes
O22	H22	O26		0.66(4)	2.06(4)	2.716(3)	173(3)	.	yes
O22	H22'	O6		0.85(3)	1.80(4)	2.618(3)	163(4)	2_666	yes
O23	H23	O21		0.77(4)	2.12(4)	2.869(3)	167(4)	.	yes
O23	H23'	O27		0.66(4)	2.11(4)	2.740(3)	163(4)	2_766	yes
O24	H24	O22		0.89(4)	1.83(4)	2.720(3)	178(4)	1_645	yes
O25	H25	O23		0.80(3)	2.12(3)	2.914(3)	173(4)	2_766	yes
O25	H25'	O5		0.87(4)	1.90(4)	2.771(3)	177(3)	.	yes
O26	H26	O21		0.80(4)	2.00(5)	2.785(3)	170(5)	2_665	yes
O26	H26'	O23		0.67(5)	2.10(5)	2.753(3)	166(5)	.	yes
O27	H27	O3		0.77(4)	1.96(4)	2.726(3)	173(4)	2_756	yes
O27	H27'	O24		0.64(4)	2.12(4)	2.765(3)	175(4)	2_856	yes
O28	H28	O4		0.79(3)	2.10(3)	2.894(2)	178(5)	2_756	yes
O28	H28'	O6		0.77(4)	2.21(4)	2.966(3)	174(4)	.	yes
C8	H8	O26		0.9900	2.4300	3.401(4)	166	.	yes
C12	H12	O2		0.9900	2.4000	3.085(3)	126	1_455	yes

====END of Crystallographic Information File